

DI-158 Design Idea

LinkSwitch-II

5 W Charger/Adapter

| Application | Device | Power Output | Input Voltage | Output Voltage | Topology |
|-----------------|----------|--------------|---------------|----------------|----------|
| Charger/Adapter | LNK616PG | 5 W | 85 – 265 VAC | 5 V | Flyback |

Design Highlights

- Revolutionary control concept enables very low cost, low part-count solution
 - Primary-side control eliminates secondary-side controller and optocoupler
 - Constant voltage (CV) accuracy: $\pm 5\%$
 - Constant current (CC) accuracy: $\pm 10\%$
 - Over-temperature protection with hysteretic recovery ensures safe PCB temperatures under all conditions
 - Auto-restart: output short circuit and open-loop protection
- Highly energy efficient
 - Average efficiency over load range: 74% (vs. the 67% Energy Star 2.0 requirement)
 - No-load input energy consumption: < 50 mW at 230 VAC
- Easily meets the following specifications:
 - EN55022 and CISPR-22 Class B EMI (> 10 dB margin)
 - IEC 61000-4-5 Class 3 AC line surge and IEC61000-4-2 ESD withstand to ± 15 kV.

Operation

The schematic in Figure 1 depicts the design for a 5 W universal input, constant voltage/constant current (CV/CC) charger power-supply design based on Power Integrations' LinkSwitch-II family product LNK616PG. This design is useful for battery chargers for cell phones, USB chargers, or any applications requiring a CV/CC characteristic.

In this design diodes D1 through D4 rectify the AC input. Capacitors C1 and C2 filter the rectified AC. Inductors L1 and L2, with capacitors C1 and C2 form pi (π) filters to attenuate conducted differential-mode EMI. This, in combination with Power Integrations' transformer E-shield™ technology, means EMI standard EN55022 class B compliance with wide margin, using no Y capacitor. Fusible, flameproof, wire-wound resistor RF1 provides protection against catastrophic failure and limits inrush currents during start-up.

Figure 1 shows U1 biased from an optional bias supply, which reduces no-load power consumption and improves efficiency when driving light loads. Capacitor C4 provides decoupling of U1 and its value selects the amount of cable-drop compensation.

In the CV region, the output voltage is regulated by using ON/OFF control, and is maintained by skipping switching cycles. Regulation is maintained by adjusting the ratio of enabled to disabled switching cycles. This also optimizes the efficiency of the converter over the entire load range by scaling switching losses with output load. At light loads (trickle charge) the primary current limit is reduced to decrease the transformer flux density, which minimizes audible noise. As the load current increases, the current limit is increased and fewer and fewer cycles are skipped.

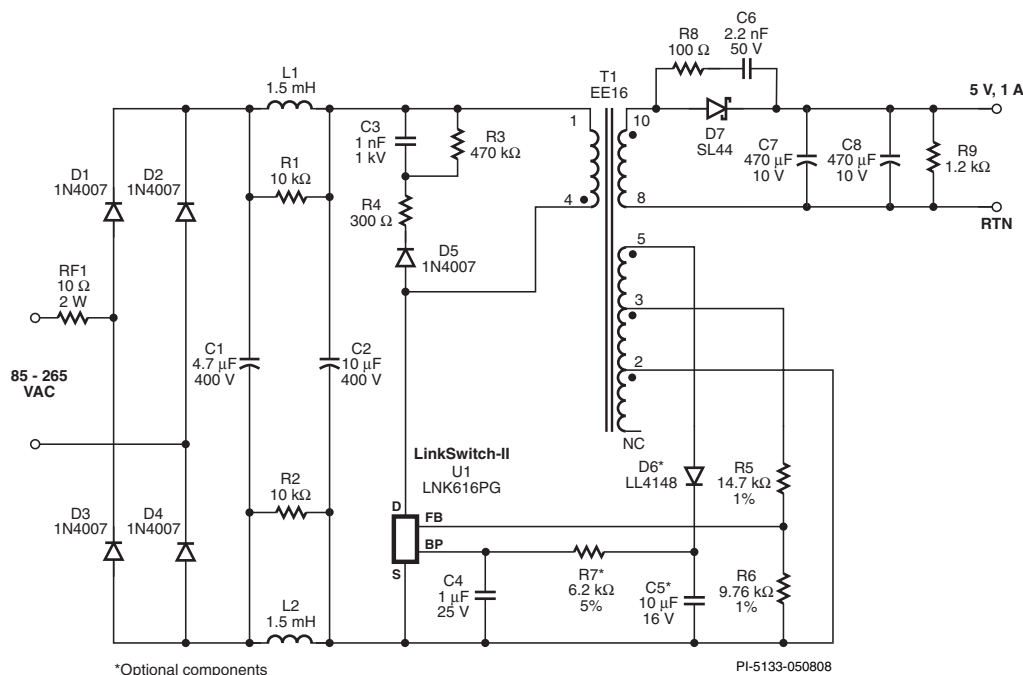


Figure 1: 5 W CV/CC Universal Input Charger Power Supply.

When no switching cycles are skipped (maximum output power point) the controller within the LinkSwitch-II transitions into CC mode. A further increase in the demand for load current causes the output voltage to drop. The drop in output voltage is reflected on the FB pin voltage. In response to the reduction of voltage at the FB pin, the switching frequency is reduced to achieve a linear CC output. The RCD-R clamp formed by D5, R3, R4, and C3 limits leakage inductance drain voltage spikes. Resistor R4 has a relatively large value to prevent ringing on the drain voltage waveform caused by the leakage inductance. This improves regulation and reduces EMI generation.

Diode D7 rectifies the secondary and C7 filters it. The combination of C6 and R8 limits transient voltage spikes across D7 and reduces conducted as well as radiated EMI. Resistor R9 acts as an output preload to ensure the output voltage at no-load is within acceptable limits. Feedback resistors R5 and R6 set both the maximum operating frequency (and thereby the output current) in the CC region and the output voltage in the CV region.

Key Design Points

- Capacitor C7 and C8 were chosen as a low ESR type capacitors to meet the output voltage ripple requirement without LC post filtering.
- If lower average efficiency is acceptable (3% to 4% drop), replace D7 with a PN-junction diode to lower cost. Then re-adjust R5 and R6 as needed to ensure the output voltage stays centered.
- Place C4 physically close to U1 on the PCB.
- Minimize clamp and output diode loop areas for reduced EMI.

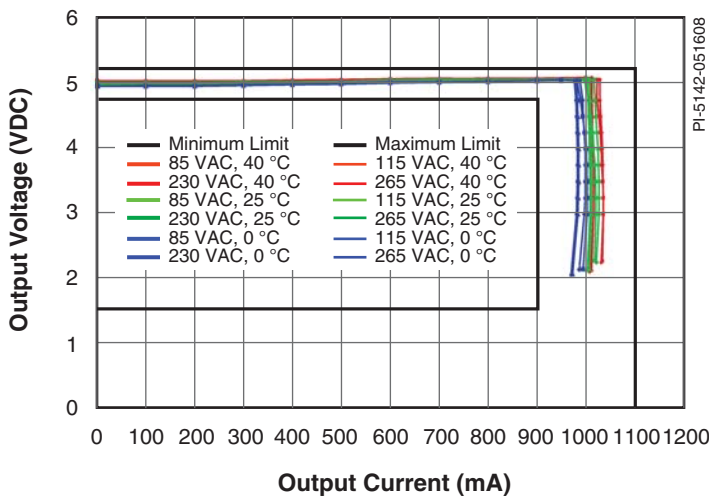


Figure 2. Typical CV/CC Characteristic Over Line and Temperature.

- Space the AC input away from switching nodes to minimize noise coupling that may bypass input filtering.
- The extended creepage distance on U1 between the high and low voltage pins prevents arcing and improves reliability, especially important in very humid conditions.
- Use 1% tolerance resistors for R5 and R6 for better output accuracy.

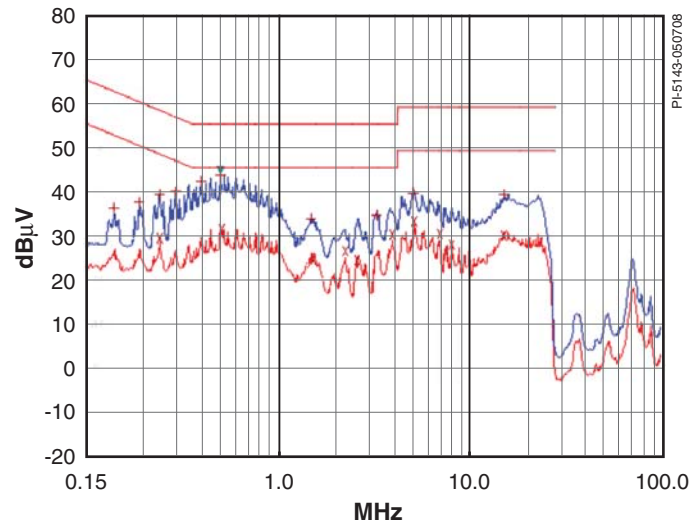


Figure 3. Conducted EMI, EN55022 B Limits: Measurements Made at 230 VAC with Output Connected to Earth Ground.

Transformer Parameters

| | |
|-----------------------------------|--|
| Core Material | EE16, NC-2H or equivalent, gapped for ALG of 88.55 nH/t ² |
| Bobbin | EE16, Horizontal, 10 pins, (5/5) |
| Winding Details | Shield: 15T x 3, 35 AWG Primary: 105T, 35 AWG 1st Half Bias: 6T x 4, 30 AWG 2nd Half /Feedback: 6T x 4, 30 AWG Secondary: 7T, 22 TIW |
| Winding Order | Shield (2-NC), Primary (4-1), Bias (5-3), Feedback (3-2), 5 V (10-8) |
| Primary Inductance | 1.074 mH, ±10% |
| Primary Resonant Frequency | 1000 kHz (minimum) |
| Leakage Inductance | 95 µH (maximum) |

Table 1. Transformer Parameters. (AWG = American Wire Gauge, TIW = Triple Insulated Wire, NC = No Connection)

Power Integrations
5245 Hellyer Avenue
San Jose, CA 95138, USA.
Main: +1 408-414-9200
Customer Service
Phone: +1-408-414-9665
Fax: +1-408-414-9765
Email: usasales@powerint.com

On the Web
www.powerint.com

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