DPA-Switch ${ }^{\circ}$

## 25 W Flyback DC-DC Converter

| Application | Device | Power Output | Input Voltage | Output Voltage | Topology |
| :--- | :--- | :--- | :--- | :--- | :--- |
| DC-DC Converter | DPA425RN | 25 W | $36-75$ VAC | 7 V | Flyback |

## Design Highlights

- Extremely low component count
- High efficiency - 85\% using Schottky rectifiers
- No current sense resistor or transformer required
- Accurate input under/over voltage meets ETSI standards
- Operates to zero load with no pre-load required
- Output overload, open loop and thermally protected
- 400 kHz operation minimizes size of magnetics


## Operation

DPA-Switch greatly simplifies the design compared to a discrete implementation. Resistor R1 programs the input under/over voltages to 33 V and 86 V , respectively. Including tolerances these thresholds guarantee the converter is operational between 36 V and 75 V , without the cost of additional line sense components.

Resistor R3 programs the internal current limit of the DPA425R to $50 \%$ of nominal. The larger DPA-Switch selection reduces conduction losses, raising efficiency without circuit changes or increased overload power.

Zener VR1 clamps leakage inductance spikes, keeping the DRAIN voltage below $\mathrm{BV}_{\text {DSs }}$. The bias supply for U 1 is provided from an auxiliary flyback transformer winding.

On the secondary, a snubber across D2 (C9, R5 and R13) limits the secondary leakage inductance spikes generated by diode reverse recovery. Inductor L2, C13 and C14 form a post-filter to reduce high frequency output switching ripple. A soft-finish network, C18, D3 and R7, eliminates output turn-on overshoot. The remaining components provide output voltage regulation and loop compensation.


Figure 1. DPA-Switch Flyback DC-DC Converter Schematic.
PI-3012-011608

## Key Design Points

- For nominal under-voltage set point $\mathrm{V}_{\mathrm{Uv}}$ : $R 1=\left(V_{\mathrm{uv}}-2.35 \mathrm{~V}\right) / 50 \mu \mathrm{~A} . \mathrm{V}_{\text {ov }}=(\mathrm{R} 1 \times 135 \mu \mathrm{~A})+2.5 \mathrm{~V}$.
- Zener VR1 voltage is 130 V to safely limit the DRAIN voltage below $\mathrm{V}_{\text {Dss }}$ of 200 V .
- Opto U2 should have a CTR of between $100 \%$ and $200 \%$ for optimum loop stability.
- Set resonance of L2 and C13 + C14 to beyond loop crossover frequency (typically 5\% to 10\% of switching frequency).
- Good layout practices should be followed:
- Locate C5, C6 and R4 close to U1, with grounds returned to the SOURCE pin.
- Primary return should be connected to the DPA-Switch tab, not the SOURCE pin.
- Minimize the primary and secondary loop areas to reduce parasitic leakage inductance.


## Transformer Parameters

| Core Material | PR1408 Siemens N87, <br> gapped for $340 \mathrm{nH} / \mathrm{t}^{2}$ |
| :--- | :--- |
| Bobbin | P1408 8 pin (B\&B B-096 or equivalent) |
| Winding Details | Primary: $6 \mathrm{~T}+6 \mathrm{~T}, 2 \times 27 \mathrm{AWG}$ <br> Secondary: $3 \mathrm{~T}, 4 \times 25 \mathrm{AWG}$ <br> Bias: $6 \mathrm{~T}, 32 \mathrm{AWG}$ |
| Winding Order <br> (pin numbers) | Primary (4-FL), tape, Bias (2-3), tape, Secondary <br> $(5,6-7,8)$, tape, Primary (FL-1), tape |
| Inductance | Primary: $49 \mu \mathrm{H}, \pm 10 \%$ <br> Leakage: $1 \mu \mathrm{H}$ (maximum) |
| Primary Resonant | 3.8 kHz (minimum) |
| Frequency |  |

Table 1. Transformer Parameters. (AWG = American Wire Gauge)


Figure 2. Efficiency vs. Output Power.

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